Multimodal Neurosurgery Force Feedback System Based on Mesh Fusion Modeling

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Virtual reality based force feedback system is spotlighted as a safe and efficient training environment to obtain surgical skills. Neurosurgery utilizes multimodal patient images for visualization of a variety of functions in head. The aim of this study is to establish a concept of multimodal neurosurgery force feedback system based on mesh fusion modeling. In the model of mesh fusion, we developed an algorithm to detect overlapped region between the multiple meshes that are obtained from multimodal images, and to determine a new boundary between the meshes. Then, the method solved interaction between the newly defined mesh boundaries using the interaction model based on a finite element method. The proposed method was implemented, and applied to both simple and patient datasets for evaluating its applicability. As a result, the method succeeded to be applied to both simple and patient datasets. Finally, we demonstrated the early stage of the surgical approach in neurosurgery. Simulation results showed a real-time simulation of brain tissue deformation with force feedback.

K e y w o r d s: virtual reality, surgical simulation, neurosurgery, finite element method, haptics

1. Introduction

Information technologies have made a great progress and increased possibility of a virtual reality (VR) based surgical simulation system for the purpose of training, pre-planning, and intra-operative support [1]. The surgical simulator simulates the physical behavior of human body and artificially stimulates human senses to create

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Received 30 December 2010; accepted 08 February 2011

an experience similar to one gained by a surgeon treating of a real patient. In surgical simulation, not only fidelity but also interactivity of physics simulation are required for visual and haptic feedback in response to a user's action. Recently, real-time simulation of physics-based tissue deformation is reported from several research groups. Sorensen applied the General Purpose Graphics Processing Unit (GPGPU) approach to a real-time spring-mass based deformation of heart for cardiac surgery simulation [2]. Kuroda simulated liver deformation using a finite element method (FEM) with the multi-finger force display [3]. Bachofen improved realism of the Hysteroscopic VR system by blood flow simulation [4].

In neurosurgery, surgeon treats fine structures in the skull with delicate force control without damaging small vessels and nerves. Recent advances in measurement methods enable detection of the fine brain structures [5]. Since the measurement methods to detect brain substances and vessels are different, the surgeon must integrate multimodal 3D images to observe the geometrical relationship of the brain structures. Surgical simulation also has to consider complicated structures obtained by multimodal images to improve realism of the simulation. Neurosurgery simulation with sole modality is less practical because the detailed structures of vessels and nerves are obtained from multimodal images. Surgical simulation has been studied as related to neurosurgery as well as other surgical fields [6–9]. For example, Hayashi proposed a system to navigate a target lesion, and Spicer proposed a simulator with multi-modality images [7]. However, the systems have never taken into consideration the force feedback and collisions of the simulated objects (i.e., meshes) as obtained from the multimodal images. Kuroda proposed a concept of neurosurgery force feedback system [10, 11]. The paper, however, focused on describing a concept of the proposed framework, and introduced an approach to solve the problem briefly [10]. On the other hand, the other paper applied an algorithm only to simple objects, not to patient datasets [11].

The aim of this study is to establish a multimodal neurosurgery force feedback system for the purpose of surgical training, pre-planning and intra-operative navigation. This paper proposes a mesh fusion model allowing multimodal brain data to use in neurosurgery simulation, describes details of the algorithm, and demonstrates the effect of the model by using not only simple but also patient datasets.

In FEM, the geometry of objects is represented as a large number of tetrahedral elements. The boundary and mechanical properties are set on each element. The set of elements are called mesh. The multiple meshes are obtained from multimodal images. Spatial overlap among the meshes requires consideration of the treatment of the overlapped regions and the mesh-mesh interaction. The proposed algorithm proceeds overlapped region between the meshes and allows interaction between the meshes by using the model of interaction between the meshes [12]. In this paper, the mesh consists of a set of tetrahedral elements to represent complicated geometry of human tissue.



Fig. 1. Concept of multimodal neurosurgery force feedback system based on mesh fusion modeling

2. Methodology

2.1. Concept

Figure 1 illustrates the concept of the multimodal neurosurgery force feedback system, which consists of the following functions:

- 1. Tool-mesh interaction with visual and haptic feedback
- 2. Mesh-mesh interaction
- 3. Visualization of deformed volumetric images

The multiple meshes for simulation are obtained from the sets of 3D images. The system measures surgeon's manipulation and updates the position of a virtual tool, i.e. surgical instrument. The mesh, i.e. tissue model, is deformed by FEM if the collision between the mesh and the tool is detected. The interaction between the meshes is considered in order to enhance accuracy and realism of the simulation. The reaction force is calculated and fed back to the user.

Figure 2 shows all procedures of the proposed simulation framework. The methods of inclusion processing and FEM with mesh interaction are described in this section.

2.2. Modeling Deformation

Physically-based deformable modeling has been widely studied [12, 13, 14]. The FEM-based model treats an object as continuum and has an advantage over simple mass-spring networks. In general, the FEM based analysis requires much computation

to solve simultaneous differential equations. If an object has N nodes that have three degrees of freedom, the model has 3N degrees of freedom and requires solution of 3N-sized simultaneous differential equations. Thus, in the past it was mainly used in off-line computation. However, the growth in computer and information technologies enabled real-time calculation of the FEM-based deformations. In this study, FEM is applied to the deformation of the brain and its detailed structures. FEM yields a stiffness matrix, **K**, and relates displacements to applied forces.

$$\mathbf{f} = \mathbf{K}\mathbf{u} \tag{1}$$

where $\mathbf{f} = (f_1 \ f_2 \ \dots \ f_n)^T$ and $\mathbf{u} = (u_1 \ u_2 \ \dots \ u_n)^T$ represent applied forces and displacements, respectively, and **K** is an *n* by *n* stiffness matrix. Eq.1 is derived from the principle of virtual work. The principle of virtual work indicates that the virtual work by force equals to the virtual strain energy by stress.

$$\mathbf{U} - \mathbf{W} = \mathbf{0} \tag{2}$$

where **U**, **W** represent virtual strain and virtual work, respectively. The energy conservation is applied to the mesh-mesh interaction as well.

2.3. Modeling Mesh-mesh Interaction

Interaction between objects occurs when the objects collide with each other. If energy is not lost during the collision, total energy of the two objects is preserved.



Fig. 2. Procedures of the multimodal neurosurgery force feedback system

The work by applied force is stored as strain energy. Now, we assume that a tool pushes or pulls one of the two objects, and the collision between the objects occurs as shown in Fig. 3. Figure 3(a) and Figure 3(b) show inclusion and non-inclusion types, respectively. The visualization of deformed volumetric data is realized by sliced-based volume rendering for real-time and high quality visualization. The volumetric data is reconstructed from the slices obtained by measurement methods, e.g. Magnetic Resonance Imaging (MRI) and X-ray Computed Tomography (CT).

2.4. Inclusion Processing

If multiple meshes exist in a space, the spatial relationship between the multiple meshes can be categorized into two types as shown in Figure 3. Figure 3(a) has no overlapped region between the meshes, while Figure 3(b) has the overlapped region.



Fig. 3. Inclusion relationship between multiple meshes: a) no overlapped region exits, b) an overlapped region exists

Figure 4(a) illustrates the case of no overlapped region between the meshes. If there is no spatial overlap between the meshes, mechanical properties represented by each mesh are utilized for physical simulation. The work by applied forces is stored as strain energy of meshes. Figure 4(b) illustrates the case of an overlapped region between meshes.



Fig. 4. Spatial representation and interaction between the multiple meshes: (a) the case of no overlapped region and (b) the case of an overlapped region, where Ω_A , Ω_B are the regions of the objects A and B, respectively

As shown in Figure 5, the inclusion between the meshes is treated as the following process: priority setting, inclusion decision, and new boundary setting.



Fig. 5. Procedures in inclusion solution

If there is a spatial overlap between the meshes, the priority between the meshes is set for the overlapped region to represent the mechanical properties in the space properly.

The mesh that is obtained for fine vessel structure represents the property in the space properly. For example, if the mesh of brain substance by MRI imaging (called brain mesh below) has any overlapped region with the mesh of vessel (called vessel mesh below), the vessel mesh represents the functional structure in the space in comparison with the brain mesh. Hence, in this case, the priority of the vessel mesh is set higher than the brain mesh.

Next, new boundary is defined, if the overlapped region exists. As a result, the work of the force applied by the user is stored as strain energy of both colliding meshes through the new defined boundary. The alternative way is the reconstruction of meshes to remove the overlapped region, instead of setting a new boundary. However, this solution is computationally expensive. This study takes an approach of setting a new boundary.

2.5. Algorithm

In this section, we describe how to define a new boundary with the colliding meshes. Here, inclusion relationship of the meshes A and B is examined. Concretely, the triangles of the mesh A in the tetrahedron that has intersected triangles with the surface triangles of the mesh B are registered as a possible new boundary, if the triangles are outside the mesh B. Figure 6 illustrates the elements intersected between the meshes A and B in two dimensions, and the new boundary defined by the algorithm. In this study, geometrical reconstruction of removing the overlapped region from the mesh A is not carried out, under the assumption that a small mesh representing fine structures, such as vessels and nerves, is located inside a large mesh representing brain substance, and then the effect of the overlapped region in the mesh A is small.

The description and pseudo code of the algorithm for inclusion decision are described below.

- 1. Priority is set on a pair of meshes. Here, the priority of the mesh B is set higher than that of the mesh A.
- 2. Intersection detection of the bounding box of the meshes A and B checks possibility of intersection between the meshes. If no intersection is found,



Fig. 6. Intersected elements and a new boundary between the meshes A and B

the processing goes to the step 5. If intersection is found, then the processing goes to the step 3 for detail checking.

- 3. Intersection detection between triangles of a tetrahedral element $T_{A,i}$ and all surface triangles of the mesh B is carried out. If no intersection is found or all triangles of the tetrahedral element are intersected, the processing goes to the step 5. Otherwise, the processing goes to the step 4.
- 4. The non-intersected triangles of the tetrahedral element $T_{A,i}$ are added to the triangles of the new boundary if the triangles are outside all surface triangles of the mesh B.
- 5. The processing goes to the step 3 until all tetrahedral elements of the mesh A are processed.

Algorithm 1 Inclusion decision
Input: The set of tetrahedral elements of mesh A: $T_A =$
$\{T_{A,0}, T_{A,1}, \ldots, T_{A,n-1}\}$ and the set of surface trian-
gles of mesh B: $S_B = \{S_{B,0}, S_{B,1}, \dots, S_{B,m-1}\}.$
Output: The set of new boundary triangles of mesh A:
$S' = \{S'_0, S'_1, \dots, S'_{l-1}\}.$
$count_{max} \leftarrow 4$
$S' \leftarrow \emptyset$
for each tetrahedral element $T_{A,i}$ of mesh A do
$count \leftarrow 0$
$S_{int} \leftarrow \emptyset$
for each triangle $S_{A,i,j}$ of $T_{A,i}$ do
for each surface triangle $S_{B,k}$ of mesh B do
if $S_{A,i,j}$ intersects with $S_{B,k}$ then
$count \leftarrow count + 1$
$S_{int} \leftarrow S_{int} + \{S_{A,i,j}\}$
end if
end for
end for
if $count \neq 0 \land count \neq count_{max}$ then
for each triangle $S_{A,i,j}$ of $T_{A,i} \notin S_{int}$ do
if $S_{A,i,j}$ is outside $S_{B,k} \in S_B$ then
$S' \leftarrow S' + \{S_{A,i,j}\}$
end if
end for
end if
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The above procedure solves the situation when multiple meshes overlap with each other in a space, and defines a new boundary to consider the interaction between the meshes.

2.6. Simulation of Contact Deformation

The contact deformation between meshes is solved by the interaction model proposed in [12]. The interaction model yields virtual displacement to colliding meshes, and determines displacements of the meshes to minimize the difference of virtual stresses by using Eq. 3. As related studies, Selle proposed a method, which yields a constraint of preserving the relative velocity before and after collision of bodies [15]. However, the method never determines any contact deformation occurred in collision. Sibille and Joukhadar proposed methods to determine displacements of colliding meshes based on geometrical information, such as the barycenter and volume of the overlapped region, respectively [16, 17]. The methods, however, never take into consideration the different stiffness of two objects. On the other hand, the interaction model proposed in [12] takes into account the contact stress of colliding objects. As a result, the model represents the contact deformation that reflects mechanical properties.

The difference of virtual stress between meshes *i*, *j* is represented as

$$\left|\mathbf{E}_{i,j}\right| = \left|\boldsymbol{\sigma}_{i}(\mathbf{u}_{i}) - \boldsymbol{\sigma}_{j}(\mathbf{u}_{j})\right|$$
(3)

where \mathbf{u}_i , \mathbf{u}_j are virtual displacements in the mesh *i* and *j*, respectively, and $\mathbf{\sigma}_i$, $\mathbf{\sigma}_j$ are virtual stresses in the mesh *i* and *j*, respectively. The iteration process yields displacements \mathbf{u}_i , \mathbf{u}_j by minimizing $|\mathbf{E}_{i,j}|$.

Computational cost of real-time processing to calculate the deformation and force can be reduced by preprocessing [18]. The displacement is calculated by using the inverse of the stiffness matrix $\mathbf{L} = \mathbf{K}^{-1}$ as shown in Eq. 4.

$$\mathbf{u} = \mathbf{L}\mathbf{f} \,. \tag{4}$$

In Figure 4, the nodes in the mesh A are categorized into the following three types: contact nodes by a user, colliding nodes with the mesh B and the other nodes. The nodes in the mesh B are categorized into the following two types: colliding nodes with the mesh A and the other nodes. The stiffness equations of objects A and B are as follows:

$$\begin{pmatrix} \mathbf{u}_{c} \\ \mathbf{u}_{b} \\ \mathbf{u}_{o} \end{pmatrix} = \begin{pmatrix} \mathbf{L}_{cc} & \mathbf{L}_{cb} & \mathbf{L}_{co} \\ \mathbf{L}_{bc} & \mathbf{L}_{bb} & \mathbf{L}_{bo} \\ \mathbf{L}_{oc} & \mathbf{L}_{ob} & \mathbf{L}_{oo} \end{pmatrix} \begin{pmatrix} \mathbf{f}_{c} \\ \mathbf{f}_{b} \\ \mathbf{f}_{o} \end{pmatrix}$$
(5)

$$\begin{pmatrix} \mathbf{u'}_{b} \\ \mathbf{u'}_{o} \end{pmatrix} = \begin{pmatrix} \mathbf{L'}_{bb} & \mathbf{L'}_{bo} \\ \mathbf{L'}_{ob} & \mathbf{L'}_{oo} \end{pmatrix} \begin{pmatrix} \mathbf{f'}_{b} \\ \mathbf{f'}_{o} \end{pmatrix}$$
(6)

where subscripts c, b, o represent nodes in contact with a user, colliding boundary nodes between the meshes and the other nodes, respectively. The displacements of

both objects are calculated by the interaction model proposed in [12]. The user's input is given as the displacement \mathbf{u}_c . Not applying force on the contact and boundary nodes yields $\mathbf{f}_o = \mathbf{f}'_o = \mathbf{0}$. Virtual forces \mathbf{f}_b , \mathbf{f}'_b are calculated, when virtual displacement \mathbf{u}_b , \mathbf{u}'_b are given in the colliding boundary nodes. The interaction model yields \mathbf{u}_b , \mathbf{u}'_b . Finally, reaction force and deformation are calculated from \mathbf{f}_c , \mathbf{u}_o , \mathbf{u}'_o . Slice-based volume rendering and the mapping of 3D texture to deformed geometry of the meshes enabled volume deformation with 3D texture [19].

3. System and Data

The system was developed for evaluation. Table 1 shows the specification of the system. Figure 7 shows the outlook of the system. We prepared a simple-shaped model and a patient model. The simple-shaped model used cubic and cylindrical objects as shown in Fig. 8. The patient model consisted of the brain substance and an artery as shown in Fig. 9. The components of the model are shown in Table 2. MRI volumetric data is reduced to $256 \times 256 \times 256$ in size, and used for volume texture. Amira by Mercury Inc., is used for mesh generation. Mechanical properties of the brain are reported by a lot of studies. In this study, we applied 1.0MPa in Young modulus and 0.4 in Poisson's ratio to the model, which parameters are within the living tissue.



Fig. 7. System overview

Item	Name		
CPU	Intel Core2 Extreme 3.0GHz (4 core)		
Main memory	6.0GB		
Graphic board	nVidia GeForce 8800GT		
Graphic display	LCD monitor		
Haptic display	SensAble PHANToM Omni		

Table 1. System specification

 Table 2. Model components: (a) simple-shaped model, (b) patient model

 a)

~)		
	Cube	Cylinder
Vertices	1812	206
Tetrahedron	8324	699
Young modulus[MPa]	1.0	0.1

b)

/		
	Brain substance	Artery
Vertices	5367	1644
Tetrahedron	25103	4449



Fig. 8. Simple objects: (a) cube, (b) cylinder, (c) cylinder placed in the cube



Fig. 9. Brain-artery objects: (a) brain substance, (b) artery, (c) artery placed in the brain substance

Figure 10 shows the result of applying the method to the cubic and cylindrical meshes. The cylindrical mesh was placed in the cubic mesh. As the overlapped region between the meshes existed, a new boundary was defined by the proposed algorithm. User pushes the cubic mesh from right to left. Figure 10 (a-c) shows the result without consideration of interaction between the meshes. No deformation of the cylindrical mesh was found. Figure 10 (d-i) shows deformation with consideration of interaction between the meshes. The deformation of the cylindrical mesh was found.



Fig. 10. Simulation result in the case of a simple object: (a-c) deformation without consideration of the mesh-mesh interaction, (d-f) deformation by pushing the cubic mesh from the right side and (g-i) from the left side with consideration of the mesh-mesh interaction

The new boundaries defined with the simple-shaped models are shown in Fig. 11. The new boundaries have non-flat surface, because the boundaries have been collected from the inner triangles of the mesh. However, the result showed that the smoothness

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of the new boundaries increased as number of vertices of the mesh increased. The new boundary defined with the patient model is shown in Fig. 12. The algorithm succeeded to define the new boundary surrounding around the artery mesh.



Fig. 11. New defined boundaries with the simple-shaped models with 195 and 1521 vertices: (a, d) meshes, (b, e) front view, (c, f) upside view



Fig. 12. New defined boundary with the patient model: (a) artery and new boundary, (b) brain substance, artery and new boundary

Figure 13 shows the relationship between iteration times and the difference of contact stresses between the boundary nodes of meshes in the case of the simple-shaped model. The result indicated that the difference of stress decreased with increasing iteration times. Figure 14 shows reaction forces with and without meshmesh interaction in the case of the simple-shaped model. The result indicated the difference of reaction forces with considering the mesh-mesh interaction.

Next, the computation time for the new boundary setting was measured when the number of nodes of the cubic mesh was changed. Table 3 shows number of the triangles of the new boundary, inside triangles of the mesh, and the ratio of the triangles of the new boundary among the inside triangles, when number of the nodes of the cubic mesh is increased. Figure 15 shows the increase of number of triangles of the new boundary and calculation time for definition of the new boundary. The new boundary setting takes several seconds. Thus, it is not a real-time computation. However, the improvement of the algorithm and pre-processing would achieve realtime computation in the future.



Fig. 13. Relationship between iteration times of interaction calculation and the difference of contact stresses



Fig. 14. Reaction forces with or without considering of interaction calculation



Fig. 15. Number of triangles of the new boundary and calculation time: (a) triangles of new boundary, (b) calculation time for definition of the new boundary

Vertices	50	107	124	195	207	291	386	483
Triangles of new boundary	38	51	57	74	64	100	125	139
Inside triangles	454	1232	1471	2448	2581	4013	5564	6937
Calculation time [ms]	83.6	169.5	194.6	323.0	345.1	518.9	731.4	902.5
Ratio [%]	8.4	4.1	3.9	3.0	2.5	2.5	2.2	2.0
Vertices	535	678	96	66 1	013	1227	1521	1812
Vertices Triangles of new boundary	535 132	678 179	96 97 21	56 1 18	013 237	1227 252	1521 289	1812 313
Vertices Triangles of new boundary Inside triangles	535 132 8043	678 179 10719	96 21 0 1573	56 1 18 34 16	013 237 5863	1227 252 20549	1521 289 26415	1812 313 32250
Vertices Triangles of new boundary Inside triangles Calculation time [ms]	535 132 8043 1035.3	678 179 10719 1385.8	96 21 21 1573 3 2029	56 1 18 34 16 .5 21	1013 237 5863 66.0	1227 252 20549 2627.0	1521 289 26415 3392.9	1812 313 32250 4116.6

Table 3. Time for defining a new boundary

Figure 16 shows the images produced by the developed system. The images show the early stage of the surgical approach in neurosurgery. The system allows user to exclude brain tissue interactively with force feedback. In Figure 16(a), a part of cerebellum is visible through a hole of the skull, and accessible by a virtual tool. In Figure 16(b), cerebellum is excluded by the virtual tool, which changes color from gray to red according to the magnitude of the reaction force. The color is set according to the formula: (R, G, B) = (min(0.2 + f, 1), max(0.2 - f, 0), max(0.2 - f, 0)), where f is the magnitude of the reaction force. Here, each color has the value ranged from 0 to 1. In Figure 16(c), (d), the skull is not visualized in the images.



Fig. 16. Simulation result with brain meshes: (a) a part of cerebellum is visible through a hole of the skull, and accessible by a virtual tool, (b) cerebellum is excluded by the virtual tool, which changes color from gray to red according to the magnitude of the reaction force, and (c),(d) the skull is not visualized in the images

4. Conclusions

This paper proposed a FEM-based mesh-mesh interaction method with the multimodal 3D meshes. The proposed method detected an overlapped region between the meshes and defined a new boundary to consider interaction between the colliding meshes. The result of the simulation indicated that the proposed method enabled definition of the new boundary between the meshes and consideration of the mesh-mesh interaction by using simple and patient datasets. The force feedback system was implemented, and applied to the early stage of the surgical approach in neurosurgery. The results showed the real-time simulation of brain tissue deformation with visual and force feedback. As a future work, the simulation of a viscoelastic tissue model and a spinal fluid model would be integrated in the system.

Acknowledgment

This study was partly supported by Grant-in-Aid for Scientific Research (S16100001) from JSPS, the Global COE Program "*in silico* medicine" at Osaka University, and Casio science promotion foundation. This study was approved by the ethical committee of School of Medicine, Asahikawa Medical University (approval number: 694).

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